



New Cost Reduction Opportunities for Adaptive Control Charts



出處：Computers & Industrial Engineering 審查中
作者：???
報告學生：陳昫名
指導老師：童超塵 教授

1. Introduction

- 適應性 (Variable-parameter - Vp) \bar{X} control charts 已被大量研究，經濟設計下之 Vp 管制圖最佳參數設計也已被建立
- 而本研究模型是基於 Nenes (2011) 的 "A new approach for the economic design of fully adaptive control charts"
- 通常 h_2 最小值為大於 0 因此， $h_2=0$ ，這是可能的，此解釋為立即抽樣
- 此篇利用此點立即抽樣可降低成本

2. Problem Setting and Assumptions

- 假設製程為常態 μ_0 and variance σ^2
- μ_0 to $\mu_1 = \mu_0 + \delta\sigma$
- μ_0 to $\mu_2 = \mu_0 - \delta\sigma$
- 直到發生可歸屬原因1 (2)假設為指數分配其 mean $1/\lambda_1$ ($1/\lambda_2$)
- 總發生可歸屬原因期望值為 $\lambda = \lambda_1 + \lambda_2$
- 假設直到發生可歸屬原因間隔 h 單位時間，則其函數為 $\gamma = 1 - \exp(-\lambda h)$

- 直到發可歸屬原因 $j(j=1 \text{ or } 2)$ ，間隔時間 h 其函數為
$$\gamma_j = \frac{\lambda_j}{\lambda} \gamma \quad j=1,2.$$

- T_0 為當假警報發生時期望搜尋時間
- T_1 蒐尋任何可歸屬原因期望搜尋時間
- T_2 恢復至管制內期望時間
- c 為變動抽樣成本
- b 是固定成本

- M 為製程運作下任何可歸屬原因單位時間成本
- L_0 假警報成本
- L_1 恢復制程管制成本
- 指標變數 δ_1 and δ_2 (0 or 1)

3. The Vp X-Shewhart chart

- $h1, n1, k1$ and $h2 = 0, n2, k2$, where $n1 \leq n2$ and $k1$
- 根據實際樣本平均值和以及臨界值 w 可做出以下決定：
 - (a) 詳細檢查修理或不用
 - (b) the size of the next sampling interval - $h1$ or 0 (immediately)
 - (c) the next sample size - $n1$ or $n2$ - and
 - (d) the next control limit - $k1$ or $k2$. Thus, there are six design parameters that affect the operation of the Vp X-Shewhart chart: $h1, n1$ and $n2, k1$ and $k2$ and w .

$$\mathbf{P} = \begin{matrix} & \begin{matrix} (0,R) & (0,T) & (0,S) & (1,R) & (1,T) & (1,S) & (2,R) & (2,T) & (2,S) \end{matrix} \\ \begin{matrix} (0,R) \\ (0,T) \\ (0,S) \\ (1,R) \\ (1,T) \\ (1,S) \\ (2,R) \\ (2,T) \\ (2,S) \end{matrix} & \left[\begin{array}{cccccc|ccc}
 p_{00}^{RR} & p_{00}^{RT} & p_{00}^{RS} & p_{01}^{RR} & p_{01}^{RT} & p_{01}^{RS} & p_{02}^{RR} & p_{02}^{RT} & p_{02}^{RS} \\
 p_{00}^{TR} & p_{00}^{TT} & p_{00}^{TS} & 0 & 0 & 0 & 0 & 0 & 0 \\
 p_{00}^{SR} & p_{00}^{ST} & p_{00}^{SS} & p_{01}^{SR} & p_{01}^{ST} & p_{01}^{SS} & p_{02}^{SR} & p_{02}^{ST} & p_{02}^{SS} \\
 \hline
 0 & 0 & 0 & p_{11}^{RR} & p_{11}^{RT} & p_{11}^{RS} & 0 & 0 & 0 \\
 0 & 0 & 0 & p_{11}^{TR} & p_{11}^{TT} & p_{11}^{TS} & 0 & 0 & 0 \\
 p_{10}^{SR} & p_{10}^{ST} & p_{10}^{SS} & p_{11}^{SR} & p_{11}^{ST} & p_{11}^{SS} & p_{12}^{SR} & p_{12}^{ST} & p_{12}^{SS} \\
 \hline
 0 & 0 & 0 & 0 & 0 & 0 & p_{22}^{RR} & p_{22}^{RT} & p_{22}^{RS} \\
 0 & 0 & 0 & 0 & 0 & 0 & p_{22}^{TR} & p_{22}^{TT} & p_{22}^{TS} \\
 p_{20}^{SR} & p_{20}^{ST} & p_{20}^{SS} & p_{21}^{SR} & p_{21}^{ST} & p_{21}^{SS} & p_{22}^{SR} & p_{22}^{ST} & p_{22}^{SS}
 \end{array} \right] \end{matrix}$$

- 製程在管制內時 $(0, R)$ 表示較寬的參數 $(0, T)$ 表示較窄的參數，下一個抽樣則為 $(0, S)$
- 而在 $(0, T)$ 之後是採取立即抽樣，因此並無可歸屬原因發生
- p_{klij} ($i, j \equiv \{R, T, S\}$ and $k, l = \{0, 1, 2\}$)

■ 期望週期時間成本

$$EC = \pi_{0R} \cdot \left(M \left(h - \frac{\gamma}{\lambda} \right) + b + cn_1 \right) + \pi_{0S} \cdot \left(L_0 + M \left(h - \frac{\gamma}{\lambda} \right) + b + cn_1 \right) + (\pi_{1R} + \pi_{2R}) \cdot (Mh + b + cn_1) + (\pi_{0T} + \pi_{1T} + \pi_{2T}) \cdot cn_2 + (\pi_{1S} + \pi_{2S}) \cdot \left(L_1 + M \left(h - \frac{\gamma}{\lambda} + \delta_1 T_1 + \delta_2 T_2 \right) + b + cn_1 \right)$$

■ 期望週期時間

$$ET = (\pi_{0R} + \pi_{1R} + \pi_{2R} + \pi_{0S} + \pi_{1S} + \pi_{2S})h + (1 - \delta_1)T_0 \cdot \pi_{0S} + (T_1 + T_2) \cdot (\pi_{1S} + \pi_{2S}).$$

- 期望週期單位時間成本 $ECT = EC / ET$

4. Numerical Investigation

- k_1 and k_2 值大約都增加或降低0.1左右
- h_1 大約增加0.1左右
- 比較原模型所節省成本約為0.3~8.3%
- 當偏移量越大，且M與 L_0 越大時，所節省的成本更多
- $b=5$ 時比起 $b=0$ (case 1 對 5, 2 對 6 以此類推) 所節省的成本更多

Table 1: 參數設定32個案例($c = 1, L_1 = 200, T_0 = T_1 = T_2 = 0, \delta_1 = \delta_2 = 0$)

| Case | b | M | L_0 | λ | λ_1 | λ_2 | δ |
|---------|-----|------|-------|-----------|-------------|-------------|-----------|
| 1 (17) | 0 | 100 | 100 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 2 (18) | 0 | 100 | 200 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 3 (19) | 0 | 1000 | 100 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 4 (20) | 0 | 1000 | 200 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 5 (21) | 5 | 100 | 100 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 6 (22) | 5 | 100 | 200 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 7 (23) | 5 | 1000 | 100 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 8 (24) | 5 | 1000 | 200 | 0.01 | 0.005 | 0.005 | 0.5 (1.0) |
| 9 (25) | 0 | 100 | 100 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 10 (26) | 0 | 100 | 200 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 11 (27) | 0 | 1000 | 100 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 12 (28) | 0 | 1000 | 200 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 13 (29) | 5 | 100 | 100 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 14 (30) | 5 | 100 | 200 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 15 (31) | 5 | 1000 | 100 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |
| 16 (32) | 5 | 1000 | 200 | 0.1 | 0.05 | 0.05 | 0.5 (1.0) |

k_1 and k_2 值大約都增加或降低0.1左右， h_1 大約增加0.1左右

比較原模型所節省成本約為0.3~8.3%

Vp \bar{X} - Shewhart and Vp \bar{X} - EWMA charts for the 2.2 numerical

當偏移量越大，且M與L0越大時，所節省的成本更多

| Case | Vp \bar{X} - Shewhart ($h_2 = 0.1$ in all cases) | | | | | | | Vp \bar{X} - Shewhart ($h_2 = 0.0$ in all cases) | | | | | | | $\frac{ECT_{Vp-S} - ECT'_{Vp-S}}{ECT_{Vp-S}} \times 100\%$ | |
|------|---|-------|-------|-------|-------|-----|--------------|---|-------|-------|-------|-------|-----|---------------|--|--|
| | h_1 | n_1 | n_2 | k_1 | k_2 | w | ECT_{Vp-S} | h_1 | n_1 | n_2 | k_1 | k_2 | w | ECT'_{Vp-S} | $\times 100\%$ | |
| 1 | 6.2 | 18 | 25 | 2.2 | 2.0 | 1.2 | 11.17 | 6.1 | 17 | 26 | 2.3 | 2.0 | 1.2 | 11.12 | 0.4 | |
| 2 | 6.5 | 20 | 33 | 2.7 | 2.3 | 1.3 | 11.49 | 6.4 | 18 | 30 | 2.7 | 2.3 | 1.2 | 11.41 | 0.7 | |
| 3 | 1.7 | 16 | 26 | 2.3 | 2.0 | 1.2 | 31.76 | 1.8 | 17 | 27 | 2.4 | 2.1 | 1.2 | 31.4 | 1.1 | |
| 4 | 1.9 | 22 | 37 | 2.8 | 2.3 | 1.4 | 32.88 | 2.1 | 22 | 35 | 2.9 | 2.4 | 1.3 | 32.24 | 1.9 | |
| 5 | 7.7 | 23 | 28 | 2.1 | 1.9 | 1.3 | 12.05 | 7.9 | 23 | 28 | 2.1 | 2.0 | 1.3 | 12.01 | 0.3 | |
| 6 | 8.1 | 24 | 34 | 2.5 | 2.3 | 1.3 | 12.36 | 8.0 | 23 | 35 | 2.6 | 2.3 | 1.3 | 12.3 | 0.5 | |
| 7 | 2.0 | 20 | 29 | 2.2 | 2.0 | 1.3 | 34.79 | 2.3 | 22 | 31 | 2.3 | 2.1 | 1.3 | 34.39 | 1.1 | |
| 8 | 2.2 | 23 | 38 | 2.7 | 2.3 | 1.4 | 35.56 | 2.4 | 23 | 36 | 2.8 | 2.4 | 1.3 | 35.03 | 1.5 | |
| 9 | 2.2 | 15 | 19 | 1.9 | 1.8 | 1.1 | 44.88 | 2.6 | 17 | 20 | 1.9 | 1.8 | 1.1 | 44.49 | 0.9 | |
| 10 | 2.6 | 20 | 26 | 2.3 | 2.0 | 1.2 | 46.26 | 2.8 | 20 | 26 | 2.3 | 2.0 | 1.2 | 45.82 | 1.0 | |
| 11 | 0.7 | 19 | 24 | 2.0 | 1.9 | 1.1 | 113.03 | 0.6 | 17 | 25 | 2.3 | 2.0 | 1.2 | 111.17 | 1.6 | |
| 12 | 0.7 | 22 | 33 | 2.4 | 2.1 | 1.3 | 117.79 | 0.6 | 18 | 33 | 2.8 | 2.3 | 1.3 | 114.17 | 3.1 | |
| 13 | 2.7 | 20 | 21 | 1.8 | 1.7 | 1.2 | 47.05 | 3.2 | 21 | 21 | 1.7 | 1.7 | 1.2 | 46.62 | 0.9 | |
| 14 | 3.0 | 23 | 28 | 2.1 | 2.0 | 1.3 | 48.35 | 3.4 | 25 | 29 | 2.2 | 2.0 | 1.3 | 47.88 | 1.0 | |
| 15 | 0.8 | 23 | 26 | 1.9 | 1.9 | 1.2 | 121.02 | 0.8 | 23 | 29 | 2.1 | 2.0 | 1.3 | 120.1 | 0.8 | |
| 16 | 0.9 | 27 | 35 | 2.3 | 2.2 | 1.3 | 125.48 | 0.8 | 23 | 35 | 2.6 | 2.3 | 1.3 | 122.95 | 2.0 | |



| | | | | | | | | | | | | | | | |
|----|-----|----|----|-----|-----|-----|-------|-----|---|----|-----|-----|-----|-------|-----|
| 17 | 3.3 | 5 | 10 | 3.2 | 2.6 | 1.3 | 6.87 | 2.8 | 4 | 9 | 3.4 | 2.6 | 1.3 | 6.79 | 1.2 |
| 18 | 3.1 | 5 | 11 | 3.5 | 2.8 | 1.4 | 6.95 | 2.8 | 4 | 10 | 3.8 | 2.9 | 1.3 | 6.85 | 1.4 |
| 19 | 0.9 | 5 | 10 | 3.0 | 2.5 | 1.4 | 18.02 | 0.9 | 4 | 10 | 3.6 | 2.8 | 1.3 | 17.2 | 4.6 |
| 20 | 1.0 | 5 | 12 | 3.4 | 2.8 | 1.4 | 18.28 | 0.9 | 4 | 10 | 3.9 | 2.9 | 1.3 | 17.32 | 5.3 |
| 21 | 5.3 | 8 | 12 | 2.8 | 2.5 | 1.5 | 8.26 | 5.3 | 8 | 12 | 2.9 | 2.6 | 1.5 | 8.22 | 0.5 |
| 22 | 5.5 | 9 | 14 | 3.1 | 2.8 | 1.6 | 8.33 | 5.3 | 8 | 13 | 3.2 | 2.8 | 1.5 | 8.27 | 0.7 |
| 23 | 1.2 | 7 | 13 | 2.9 | 2.6 | 1.6 | 22.87 | 1.6 | 8 | 13 | 3.2 | 2.8 | 1.5 | 21.83 | 4.5 |
| 24 | 1.3 | 7 | 14 | 3.2 | 2.7 | 1.6 | 22.88 | 1.6 | 8 | 14 | 3.5 | 3.0 | 1.5 | 21.93 | 4.2 |
| 25 | 1.2 | 5 | 9 | 2.8 | 2.4 | 1.3 | 34.18 | 1.2 | 5 | 9 | 2.9 | 2.5 | 1.3 | 33.75 | 1.3 |
| 26 | 1.3 | 6 | 10 | 3.0 | 2.5 | 1.4 | 34.62 | 1.2 | 5 | 9 | 3.2 | 2.6 | 1.3 | 34.08 | 1.6 |
| 27 | 0.4 | 7 | 11 | 2.6 | 2.4 | 1.4 | 72.76 | 0.3 | 4 | 9 | 3.4 | 2.7 | 1.2 | 67.97 | 6.6 |
| 28 | 0.4 | 7 | 12 | 2.9 | 2.6 | 1.4 | 74.75 | 0.3 | 5 | 11 | 3.7 | 2.9 | 1.4 | 68.52 | 8.3 |
| 29 | 1.7 | 8 | 10 | 2.5 | 2.3 | 1.5 | 37.86 | 2.1 | 9 | 11 | 2.6 | 2.4 | 1.5 | 37.45 | 1.1 |
| 30 | 1.7 | 8 | 12 | 2.8 | 2.5 | 1.6 | 38.31 | 2.1 | 9 | 12 | 2.8 | 2.6 | 1.5 | 37.77 | 1.4 |
| 31 | 0.6 | 10 | 12 | 2.5 | 2.4 | 1.5 | 84.38 | 0.5 | 8 | 12 | 2.9 | 2.6 | 1.5 | 82.24 | 2.5 |
| 32 | 0.6 | 10 | 14 | 2.8 | 2.6 | 1.6 | 85.90 | 0.5 | 8 | 13 | 3.3 | 2.8 | 1.5 | 82.79 | 3.6 |

5. Summary and Conclusions

- 通過例子，此模式可降低成本，雖然幅度並不明顯
- 使用新模式在實際使用時簡單，因為它少了一個參數設計



THE END